



**CHALLENGES FACING ELECTROCHEMICAL  
DEPOSITION IN WAFER LEVEL PACKAGING**

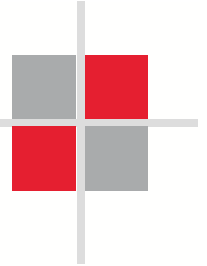
**MAY 2016**



**THOMAS B. RICHARDSON, Ph.D.**

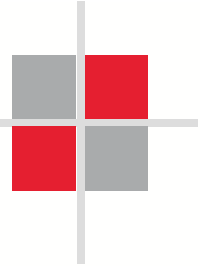


# Executive Summary



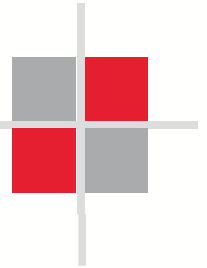
- **Mobile devices are a leading driver to growth in the IC market, specifically WLP and FC**
  - *WLP expected to grow ~20% CAGR*
- **Enthone focused on leveraging core IP in Cu electrodeposition to various applications and packaging schemes**
  - *Enthone has ~70% of Cu electroplating market share*
- **Copper plating (bump,pillar,RDL,via fill) focus of current business and New Product Development**
- **Copper plating market is becoming fragmented due to various packaging schemes and requirements for Cu.**
  - *Customization of chemistries and collaboration with tool vendor becoming a requirement*
- **New Product Development considers coplanarity, bump shape, Kirkendall voids, and plating rate as essential attributes**
- **High purity films with resistance to Kirkendall voiding desirable for specific applications**

# Summary

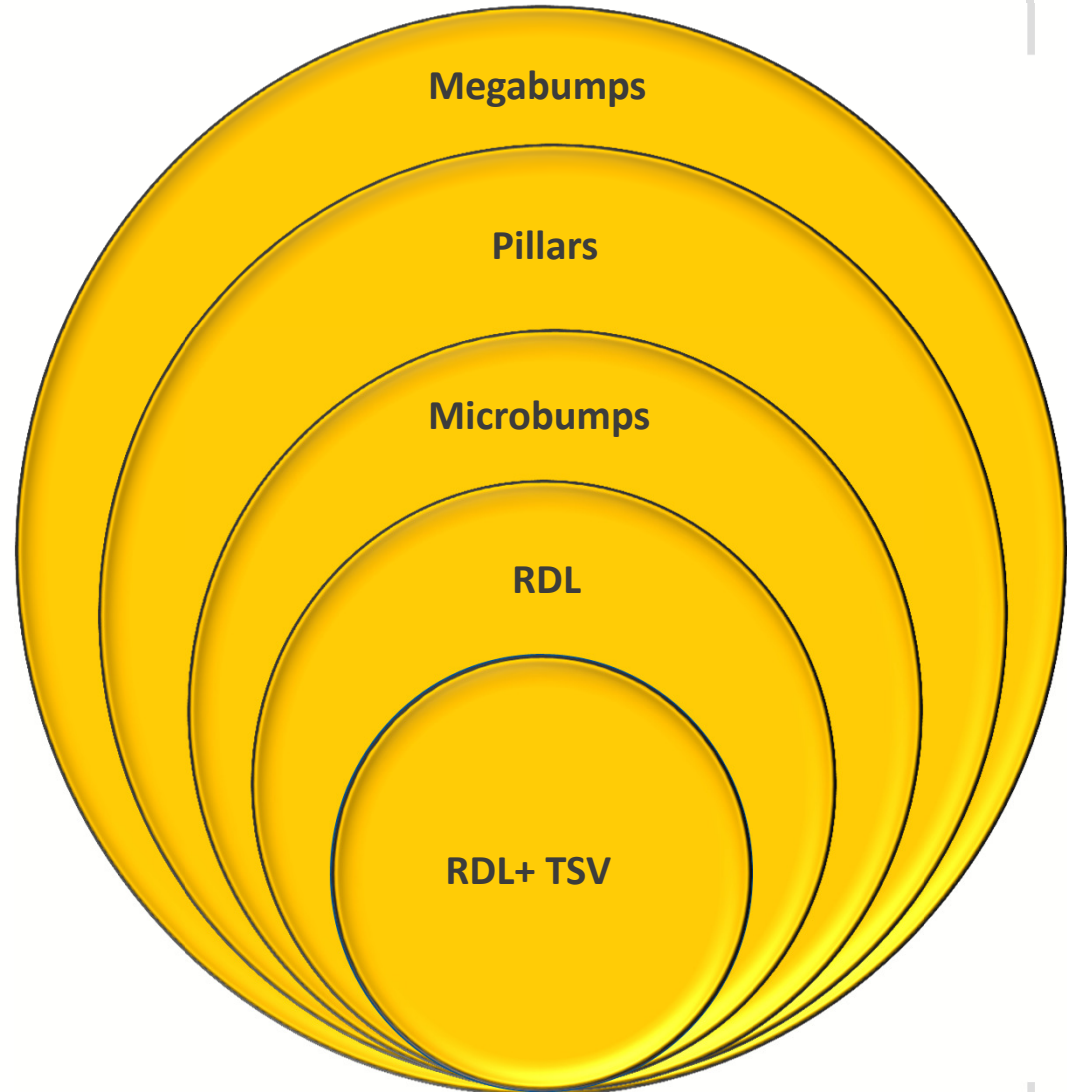


- Having a copper rich electrolyte while imperative for some processes (megabumps, pillars, TSV), may be detrimental to others (microbumps, rdl).
- Playing a critical role in nucleation, wetting properties, the relative strength of the inhibitor component plays a crucial role in establishing the bump shape. This may be important for RDL applications
- The leveler component is the corner stone of the process constantly jockeying for position with the activator component, and at times with the inhibitor as well.
  - The requirements will be application specific

# Complexity of WLP



Customers want to use a single electrolyte and additives system:  
MICROFAB SC 50  
MICROFAB SC R1  
MICROFAB SC R2 (A&B)

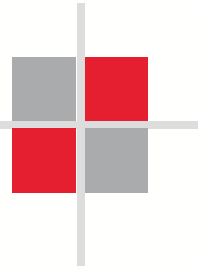


# The World of WLP



| Technology Platform | Dimensions                            | Desired Plating Rate ( $\mu\text{m}/\text{min}$ ) |
|---------------------|---------------------------------------|---|
| Megabumps           | 200x200                               | 6.0+  |
| Pillars             | 40x50                                 | 3.5   |
| Microbumps          | 20x30                                 | 3.0   |
| RDL + Via Fill      | Various Line Widths                   | 1.0- 2.0  |
| RDL + TSV + Pillar  | Various Line Widths and Aspect Ratios | TBD   |

**Market is driving a a wide range of feature sizes  
Customers want optimal performance for each**



| Attributes                    | Electrochemistry   | Primary Control Factor   | Secondary Control Factor                                     |
|-------------------------------|--|--------------------------|--|
| <b>Bump Height Uniformity</b> | High Tafel slope (Wa)  | Leveler                  | [H <sup>+</sup> ], current density, temp, [Cl <sup>-</sup> ] |
| <b>Flat Bump Shape</b>        | Minimal difference in polarization between high and low agitation ( $\Delta E$ ) | Leveler and “suppressor” | [Cu], [Cl <sup>-</sup> ], agitation                          |
| <b>Kirkendall Void-free</b>   | Non steady state Chronopotentiometry   | Leveler                  | Accelerator  |

There are many hardware and chemical “knobs” that have a direct impact to the end result

# Processes Goals

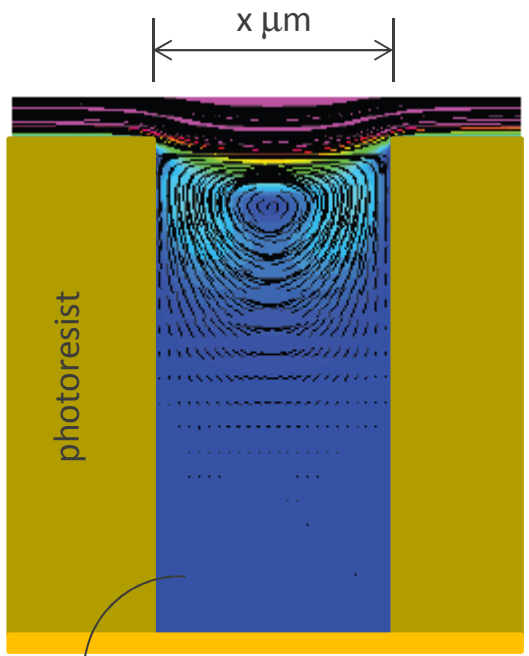
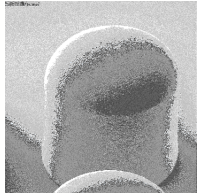


| Applications | Critical Plating Attribute   | Bump shape   |
|--------------|--|--|
| RDL          | Coplanarity  | Flat to domed on flat substrate                              |
| Microbumps   | Coplanarity  | Flat on passivation substrates, but domed on flat substrates |
| Cu Pillars   | Coplanarity at high speed ( $\geq 3.5 \mu\text{m}/\text{min}$ )          | Flat on passivation substrates, but domed on flat substrates |
| Mega Bumps   | Coplanarity, <u>Very high Throughput</u> ( $>6 \mu\text{m}/\text{min}$ ) | Flat to dished, to slightly domed on flat substrates         |

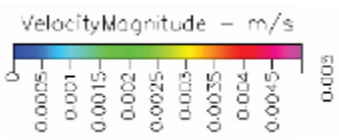
# Bump Dimension and Mass Transport



Courtesy of AMAT, Kalispell MT



Plating solution, flow velocity by color



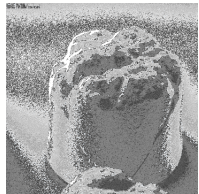
Convection zone, agitation effective depth up to opening size

Applicable current density is much higher due to sufficient mass transfer from agitation

Diffusion zone, solution velocity is zero, and all mass transport rely on diffusion

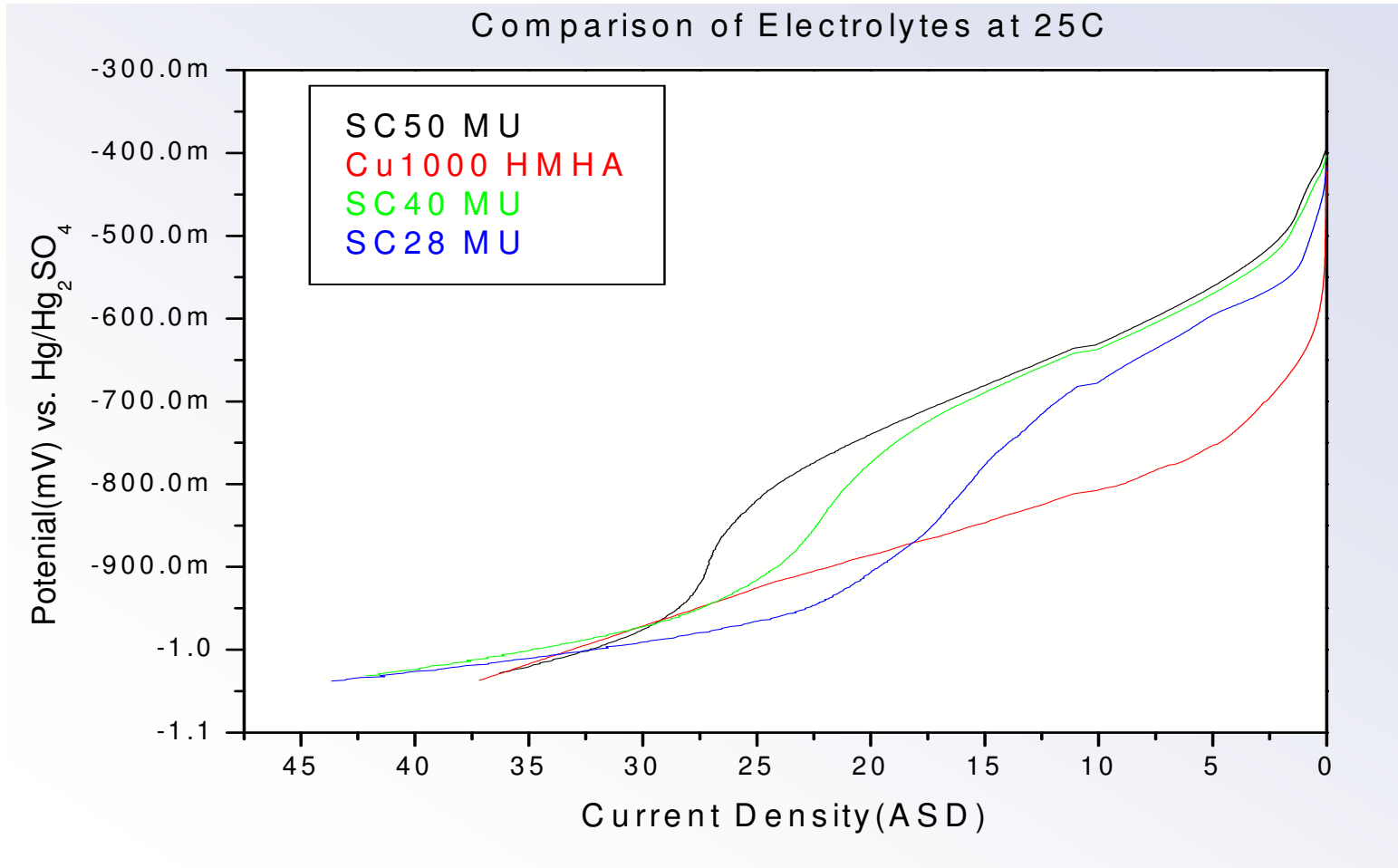
Applicable current density is limited by diffusion. Too high current density result in very domed shape or nodule in extreme case

$$i_{limiting} = \frac{nFD}{\delta} C^*$$



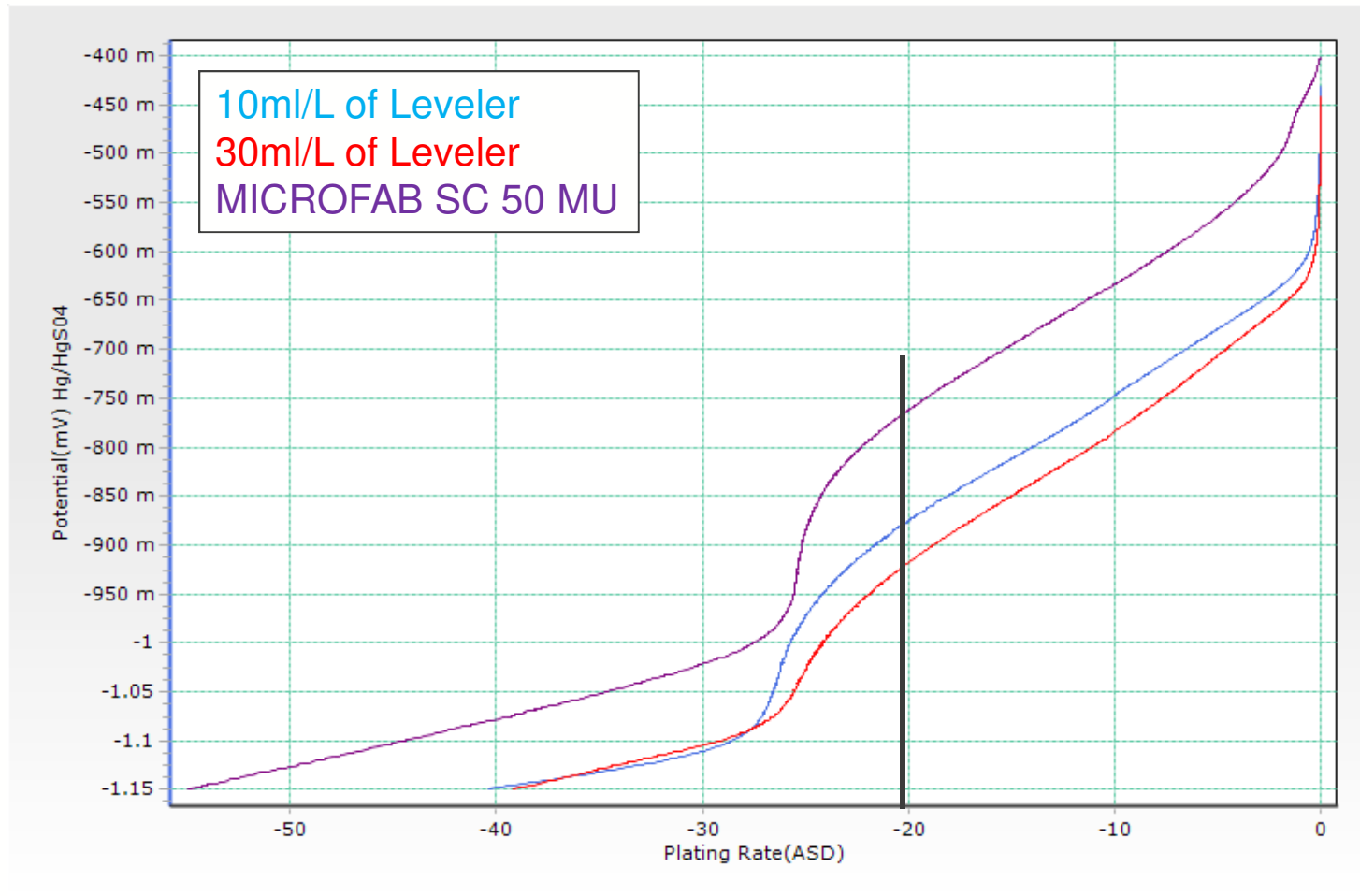
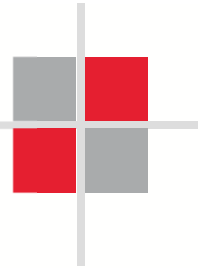


# Electrolytes Effects on Limiting Current Density



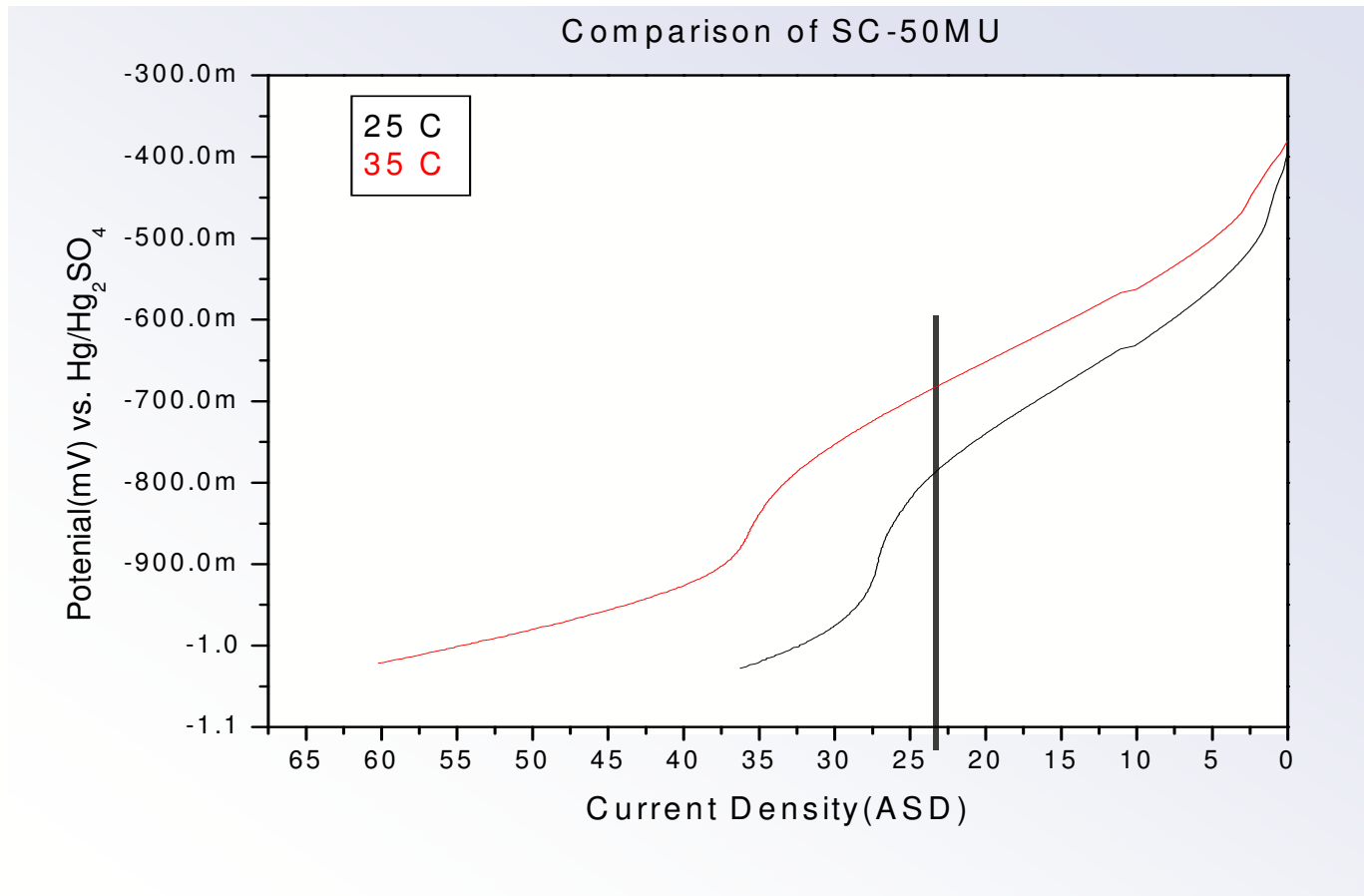
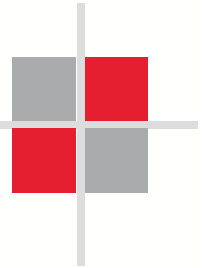
**The choice of electrolyte is important.  
It needs to be paired depending on tool platform  
and applications, i.e. TSV, RDL, Pillars, etc...**

# Additives Effects on Limiting Current: Leveler



**Additives alone do not change the limiting current.  
They govern WID and WIF uniformity.**

# Limiting Current MICROFAB SC 50 MU at 25 and 35 °C

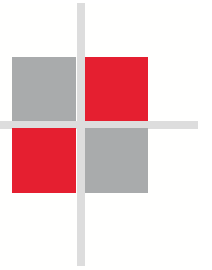


Increasing temperature increases the limiting current density.  
While 20 ASD is within the limiting current the, reaction will  
primarily be diffusion controlled.

# Summary I



- **Increasing copper ion concentration increases the limiting current of the electrolyte:**
  - *Good for TSV and Pillar*
  - *Detrimental for RDL*
- **Decreasing the concentration or lower agitation will also affect the limiting current adversely:**
  - *The lower the agitation the less mass transfer*
  - *The lower the copper concentration the lower the limiting current, which would favor RDL and yielding the best uniformity*
- **Increasing temperature increases the limiting current:**
  - *Favorable for pillar*
- **The closer the deposition rate is to the limiting current, the less additives(kinetic control) influence the copper transport (diffusion controlled).**



The role of the suppressor component:

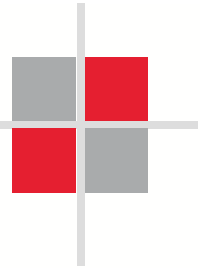
# DOES ONE FIT ALL?

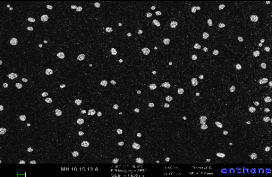
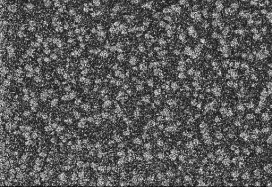
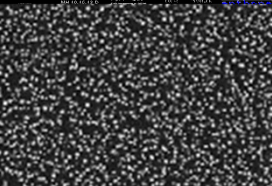
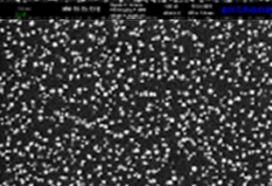
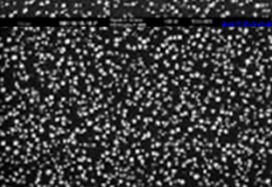
# Roles of Accelerator & Suppressor



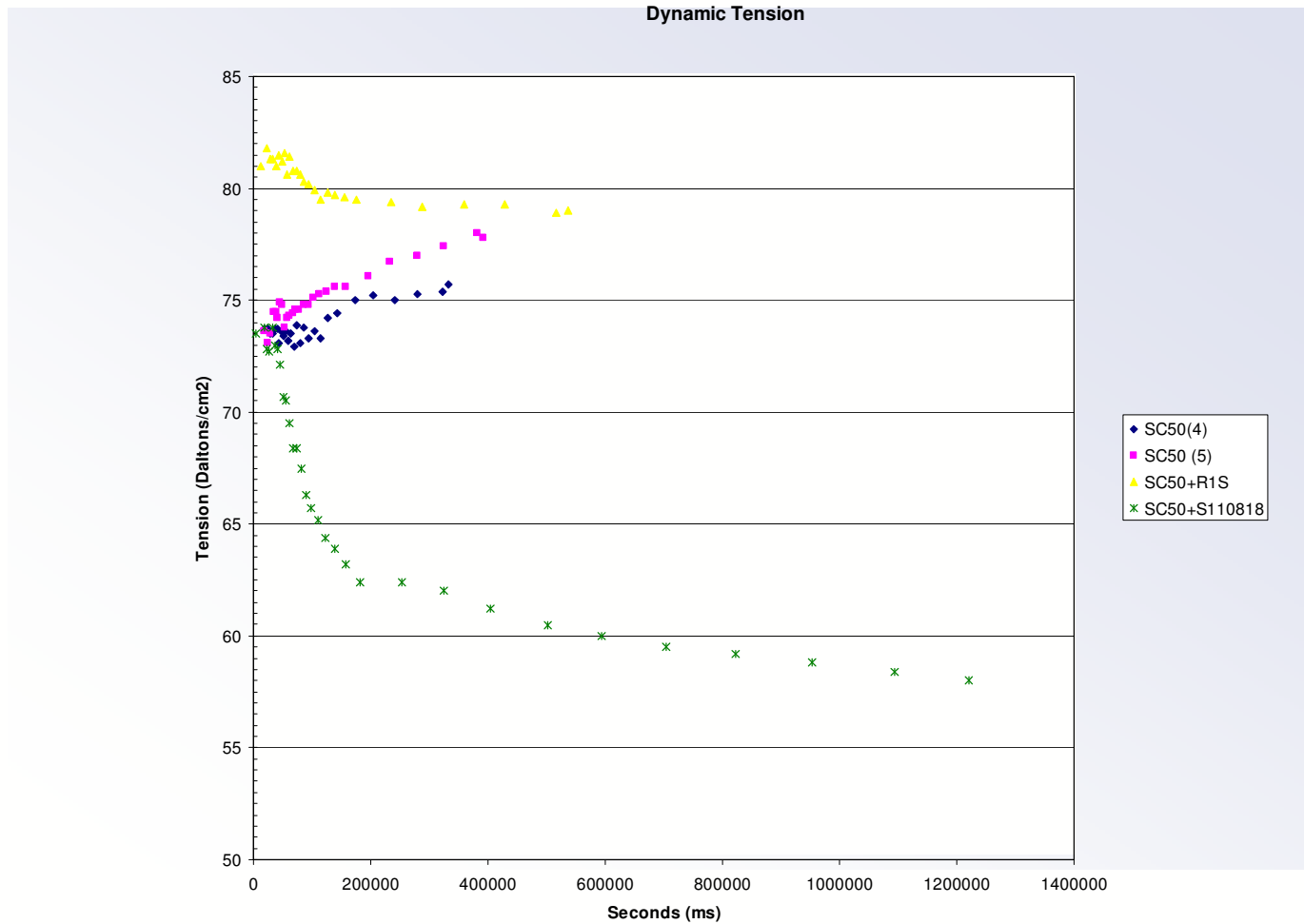
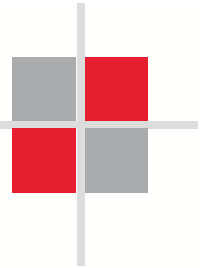
| Effect of Additives on Nucleation Density |             |                        |     |
|---|-------------|------------------------|-----|
| Suppressor (R1S)                          | Accelerator | Nuclei/cm <sup>2</sup> | SEM |
| 0   | 0           | 1.37E+08               |     |
| 0   | 20 ml/L     | 2.61E+08               |     |
| 20 mL/L                                   | 0           | 6.28E+08               |     |
| 20 mL/L                                   | 20 ml/L     | 5.34E+08               |     |

# Suppressor Role: More Important than Just Wetting



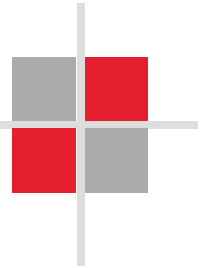
| Effect Suppressor Concentration on Nucleation Density |             |                        |   |
|---|-------------|------------------------|---|
| Suppressor Velocity BP-S                              | Accelerator | Nuclei/cm <sup>2</sup> | SEM   |
| 0   | 0           | 1.37E+08               |    |
| 20  | 0           | 6.28E+08               |    |
| 40  | 0           | 1.76E+09               |   |
| 80  | 0           | 1.10E+09               |  |
| 160   | 0           | 1.41E+09               |  |

# Suppressor Type vs. Dynamic Surface Tension



The suppressor (S110818) delivers lower surface tension than that used in MICROFAB SC R1. This is critical for high aspect ratio substrates and fine lines RDL applications.

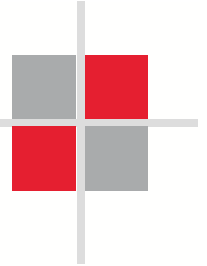




The role of the leveler:

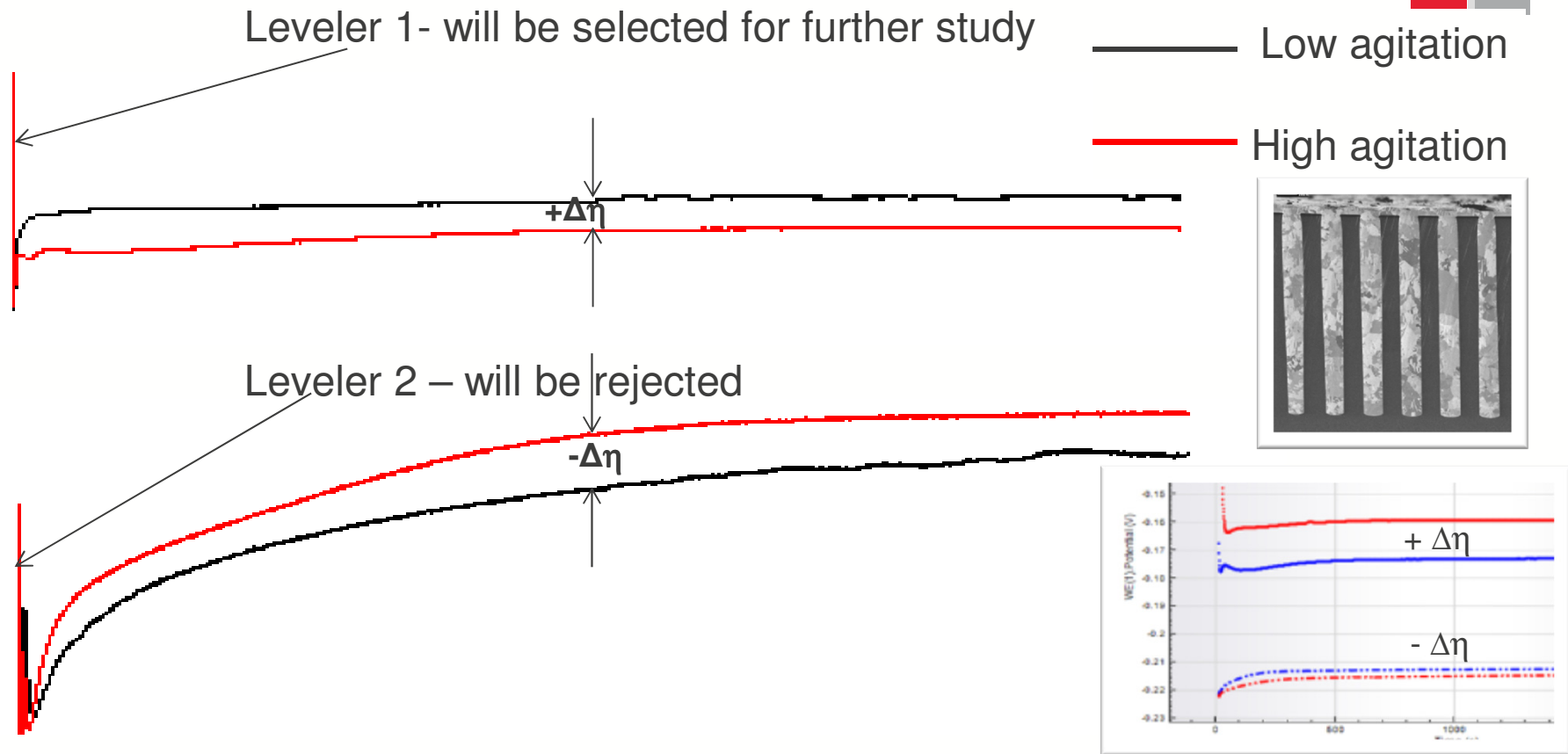
**WHAT ARE THE NECESSARY PROPERTIES OF THE LEVELER WHICH WOULD ALLOW IT TO WORK RELATIVELY WELL IN NUMEROUS SPACES: RDL; RDL+ TSV; AND PILLARS?**

# Additives Design Complexity



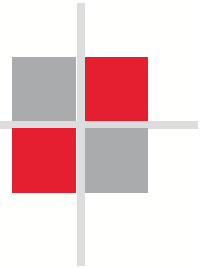
- The degree of polarization is important to obtain both bottom up fill (TSV), yet not too strong for RDL applications (bi-corn, devil horn, etc...)
- A very polarizing suppressor is adequate for RDL, but could generate poor gap fill (TSV). However, this is a good attribute for Megabumps applications.
- Too strong a leveler will cause conformal fill, undesirable for RDL, but excellent for Pillars, and Megabumps.
- There needs to be a competitive adsorption of both leveler ( High Wagner Number, appropriate  $+\Delta E$ , good mass transport) and suppressor (appropriate suppression strength and functionality) so a certain degree of polarization is maintained to counterbalance the effects of the accelerator.

# Effects of Leveler on Bottom Up Filling



$\Delta h$  value at different agitation conditions can be one of the predictors for gap fill. There is a direct correlation between the degree of separation (polarization/depolarization) and the likely bottom up fill, or a lack thereof.

# Uniformity Index: Wagner Number



**Wagner Number (Wa)** ~ Throwing Power, degree of uniformity of the macroscopic current distribution

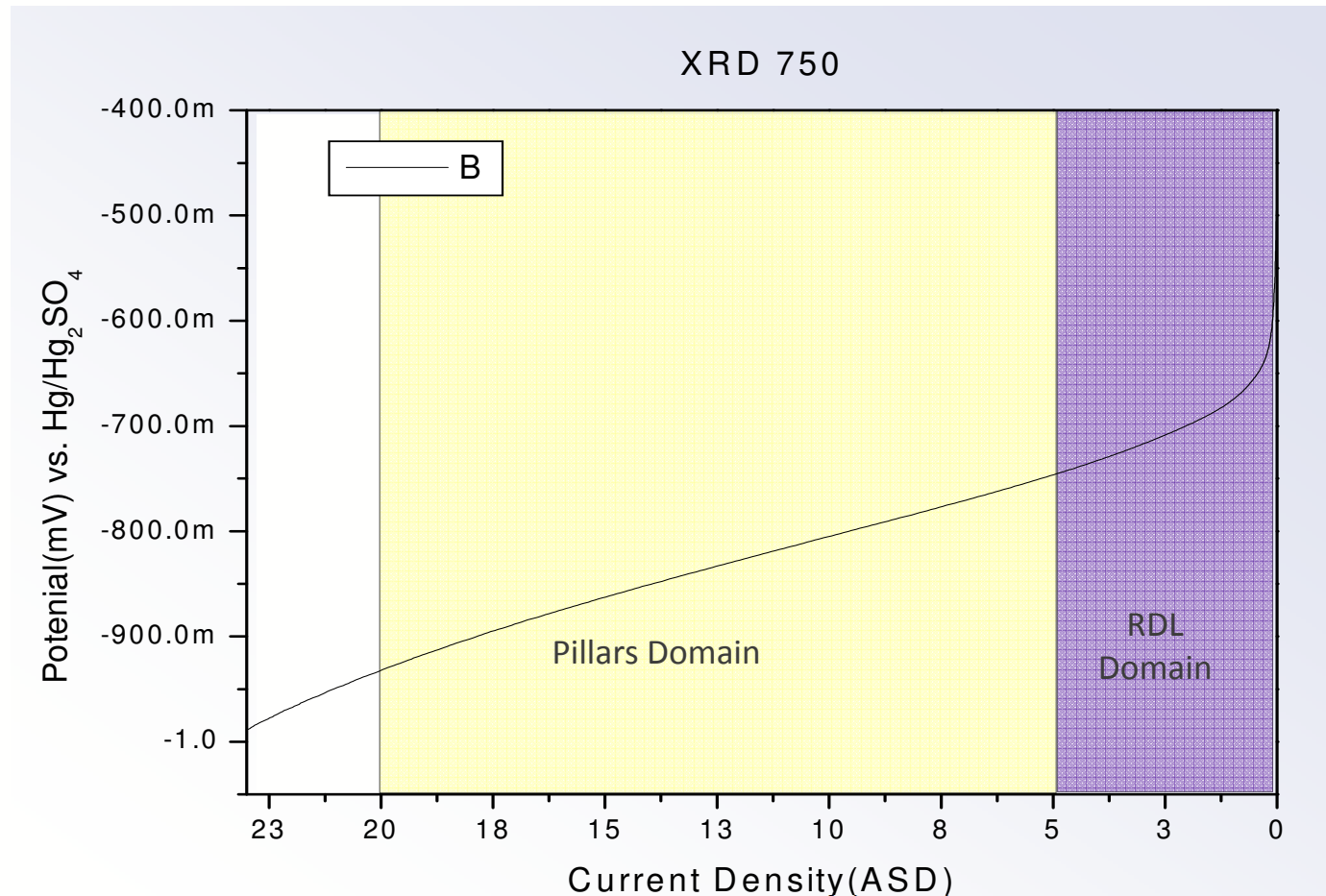
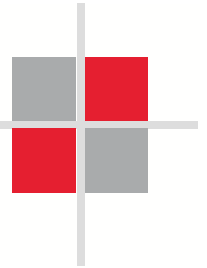
$$W_a = \frac{\text{activation resistance}}{\text{ohmic resistance}}$$
$$= \frac{R_a}{R_\Omega} = \frac{\kappa}{\ell} \left( \frac{\partial \eta_a}{\partial i} \right)$$
$$= \frac{\kappa \beta}{\ell i}$$

$\kappa$  : electrolyte conductivity  
 $\ell$  : distance between anode and cathode  
 $\beta$  : Tafel slope

**Higher Wa number, better uniformity**

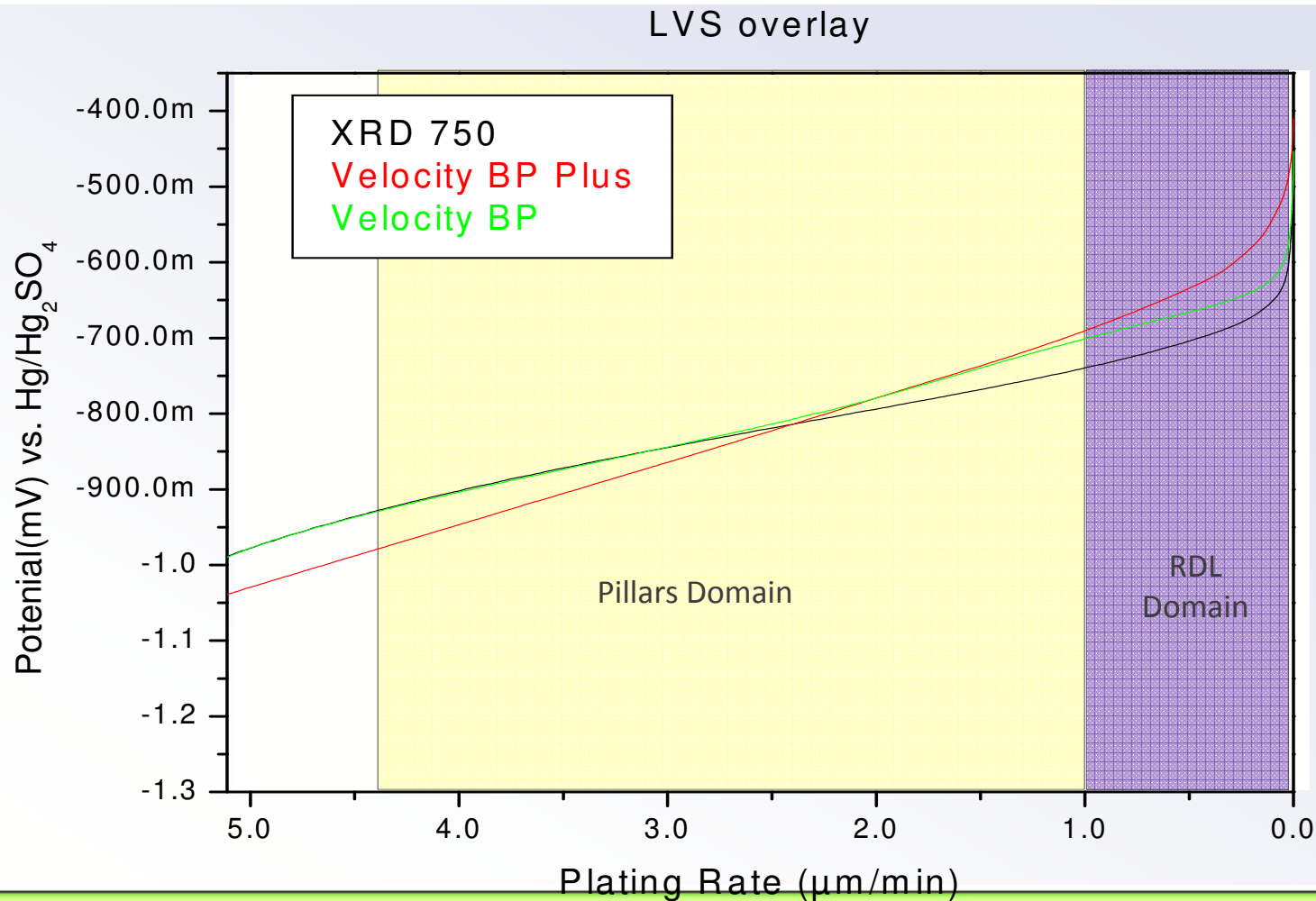
- higher  $\kappa$ : higher acid conc.
- lower  $\ell$ : closer wafer to anode distance
- higher  $\beta$ : stronger suppression from suppressor or leveler
- lower  $i$ : lower throughput

# Linear Voltammetry Sweep of a Likely 2-1 Leveler



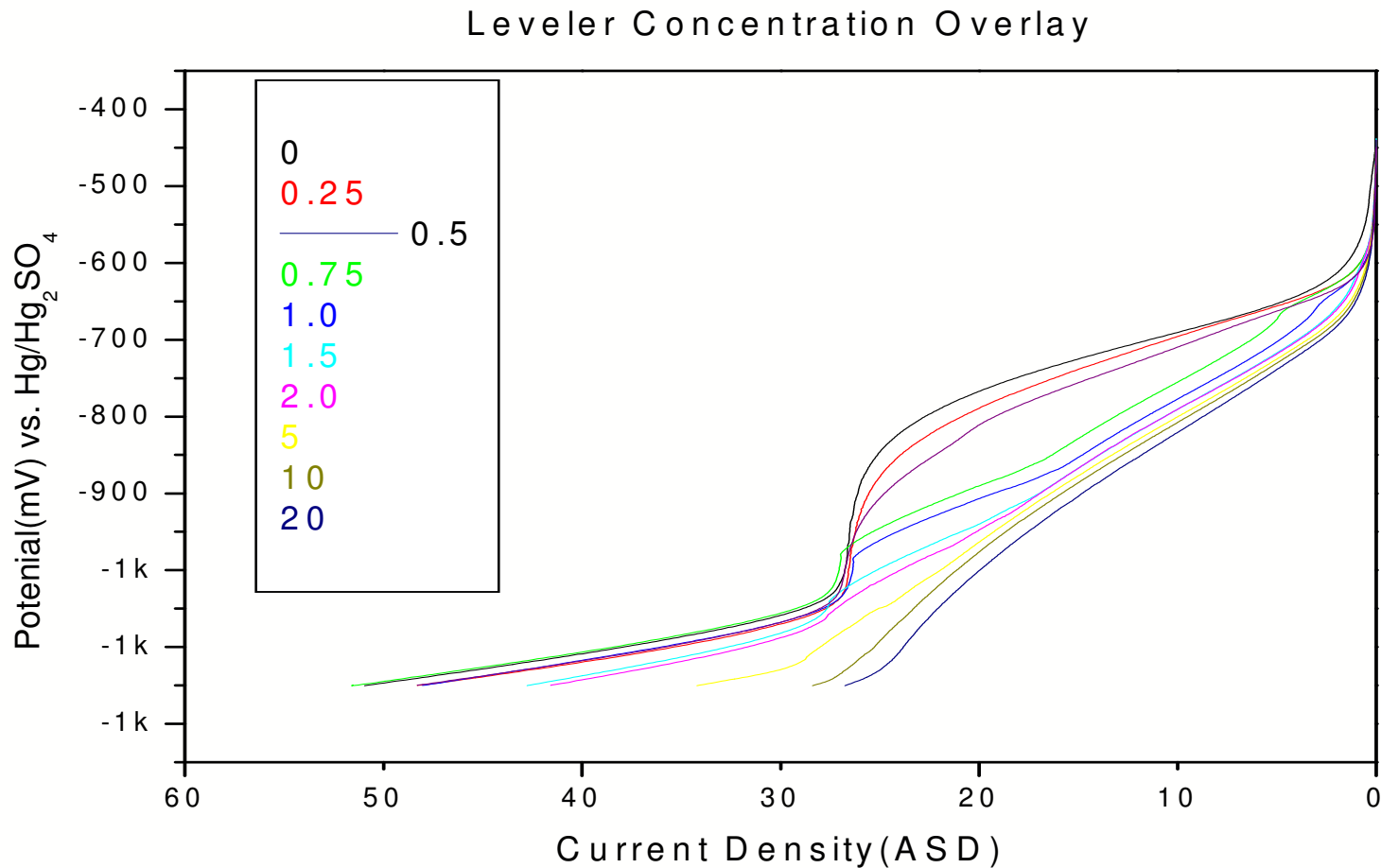
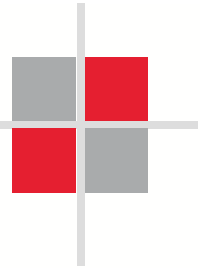
XRD 750 will perform relatively well for RDL (0.1 to 1.10 mm/min) applications having a Wa of 89. For pillar applications, acceptable performance is expected with a Wa of 50 from 1.1 to 4.4 mm/min.

# Linear Voltammetry Sweep of Various Levelers



While XRD 750 will perform relatively well for RDL and TSV applications ( $Wa= 89; 56$ ), the Velocity PLUS additives will outperform it for RDL and pillars ( $Wa= 109; 78$ ). However, the Velocity PLUS additives do not give good gap fill performance.

# Effects of Leveler Concentration on Wa



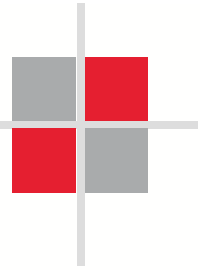
Clear change in polarization upon increasing the leveler concentration, and increased suppression as well after adding just 0.75 ml/L of leveler

# Summary II



- **The leveler component plays a critical role in achieving overall uniformity, gap fill, and controlling the bump shape:**
  - This is critical for TSV, pillars, and RDL, and megabumps
- **For RDL, the choice of suppressor is paramount in providing the necessary nucleation and achieving the proper bump shape, whereas for pillars the role of the suppressor only extend to mere, initial nucleation**
- **For RDL and microbumps, copper concentration controls the degree of doming:**
  - The lower the copper concentration, the lower the degree of doming
- **For pillars and megabumps, where throughput is of the essence, and to overcome challenging designs, a higher copper concentration of copper is desired in the electrolyte**

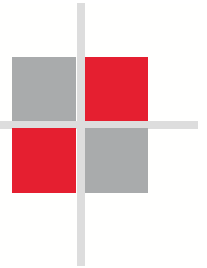




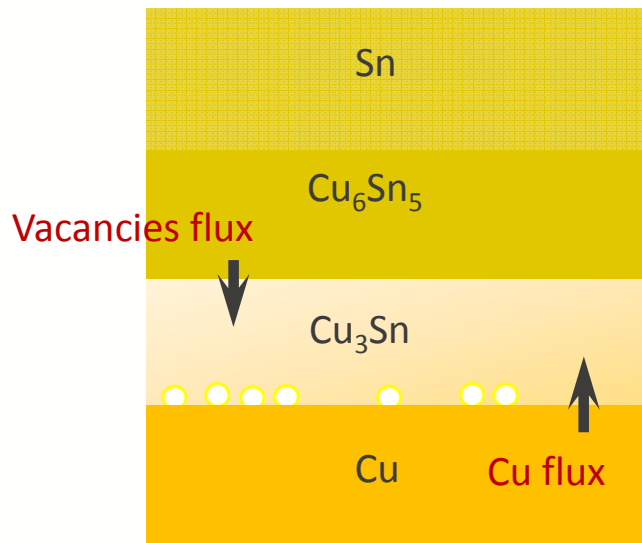
Grain size:

**HOW CAN THE GRAIN SIZE BE INFLUENCED WITH THE CHOICE OF ADDITIVES WITHOUT CHANGING THE DEPOSITION RATE? IS THERE A CORRELATION WITH UNDERSTANDING KIRKENDALL VOID FORMATION AND PREVENTION?**

# Mechanism for Kirkendall Void Formation



Cu diffusion is 3x faster than Sn



Since Kirkendall void is from diffusion

$$\tau = 2\sqrt{D \cdot t}, \quad D = D_0 e^{-\frac{E}{RT}}$$

$D$ : diffusivity

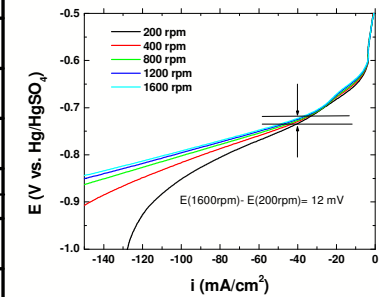
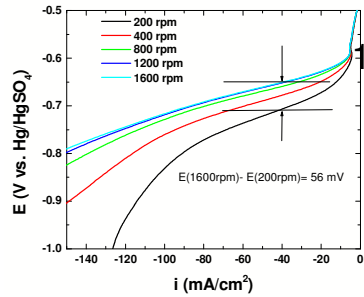
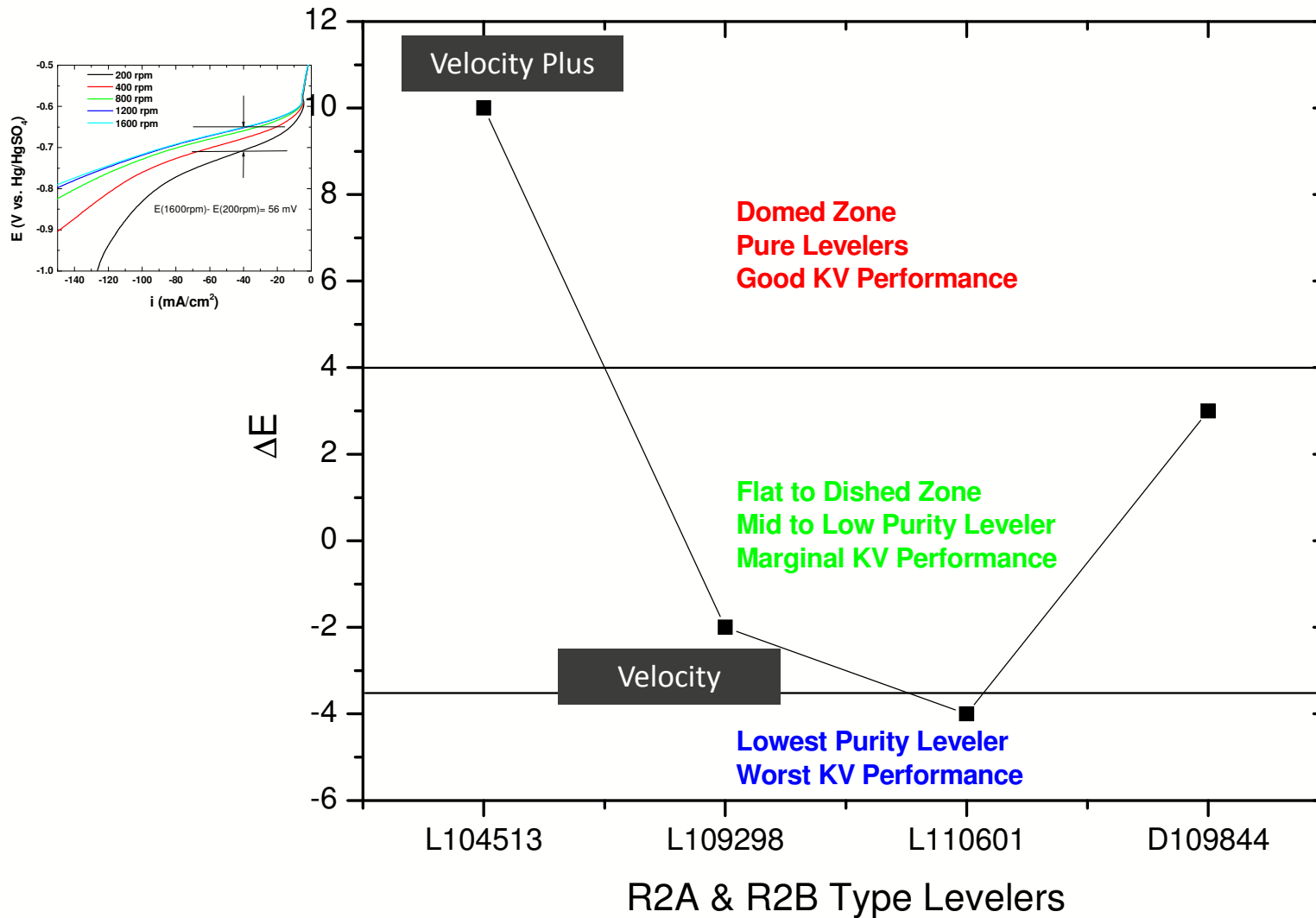
$t$ : time

$T$ : temperature

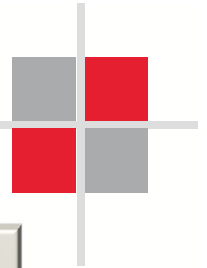
- Time and temperature are two factors in the Kirkendall void formation.

Once vacancies accumulate to super-saturation at the Cu/Cu<sub>3</sub>Sn interface, Kirkendall voids nucleate and grow.

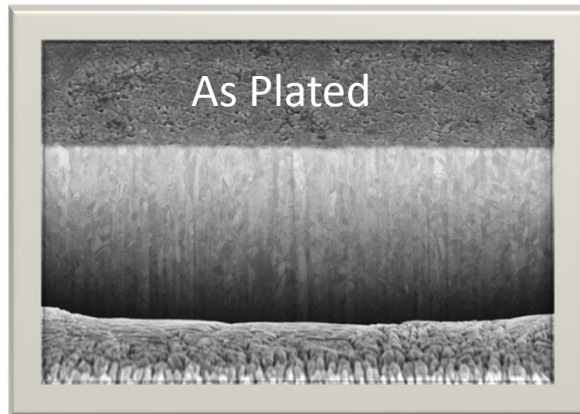
# Predicting Kirkendall Void Performance



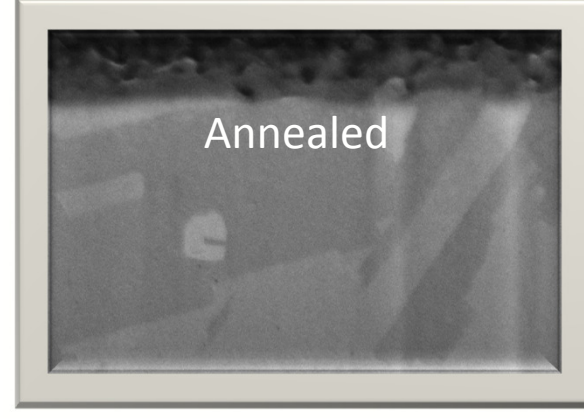
# Controlling Grain Size: Leveler Design



## Low Purity Leveler



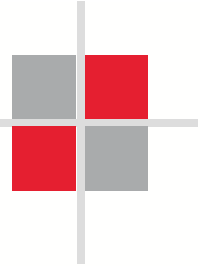
## High Purity Leveler



The average crystal size can be controlled through leveler design and its subsequent interactions with suppressor and accelerator. As such, the level of impurities in the copper film can be controlled. This will impact eventually KV performance, and perhaps etching rate.

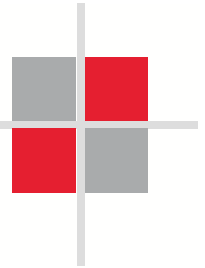
# COPPER FILM PROPERTIES

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1. Film properties of several MicroFab copper plating processes were evaluated after one dielectric bake cycle of 225°, 60 min
2. Copper films were plated at 4.54 ASD ( 1  $\mu\text{m}/\text{min}$ ), 15  $\mu\text{m}$  thickness representative of typical RDL plating speeds on Si wafers
3. Film properties such as texture, crystallite size, and stress were evaluated by X-ray Diffraction
4. Film impurities were measured by SIMS
5. Film elongation was measured by Bulge test

# POST-ANNEAL: ORIENTATION, STRESS, & CRYSTALLITE SIZE



| Index                        | Post Anneal Orientation |        |        |        |        |        | Residual Stress (MPa) Post-Anneal | Crystallite Size (Å) Post-Anneal | Total Impurity (ppm) | Pre-Anneal Bulge Test | Post-Anneal Bulge Test |
|------------------------------|-------------------------|--------|--------|--------|--------|--------|-----------------------------------|----------------------------------|----------------------|-----------------------|------------------------|
|                              | (-111)                  | (-100) | (-110) | (-311) | (-331) | (-210) |                                   |                                  |                      |                       |                        |
| <b>MICROFAB SC Process A</b> | 1%                      | 3%     | 5%     | 4%     | 22%    | 65%    | 120                               | 686                              | 157                  | 1.38                  | 4.35                   |
| <b>Times random</b>          | 0.05                    | 0.19   | 0.31   | 0.26   | 1.29   | 3.89   |                                   |                                  |                      |                       |                        |
| <b>MICROFAB SC Process B</b> | 0%                      | 0%     | 0%     | 2%     | 2%     | 95%    | 33                                | 887                              | 53.4                 | 0.53                  | 1.03                   |
| <b>Times random</b>          | 0                       | 0.01   | 0.03   | 0.12   | 0.12   | 5.72   |                                   |                                  |                      |                       |                        |
| <b>MICROFAB Process C</b>    | 3%                      | 3%     | 4%     | 6%     | 19%    | 64%    | 109                               | 856                              | 124.5                | 0.55                  | 1.00                   |
| <b>Times random</b>          | 0.15                    | 0.19   | 0.26   | 0.39   | 1.15   | 3.85   |                                   |                                  |                      |                       |                        |
| <b>MICROFAB Process D</b>    | 1%                      | 1%     | 3%     | 15%    | 13%    | 66%    | 106                               | 847                              | 2.6                  | 1.10                  | 5.13                   |
| <b>Times random</b>          | 0.08                    | 0.09   | 0.2    | 0.89   | 0.78   | 3.96   |                                   |                                  |                      |                       |                        |
| <b>Process X</b>             | 8%                      | 7%     | 11%    | 8%     | 33%    | 33%    | 114                               | 886                              | 5.5                  | 2.60                  | 4.87                   |
| <b>Times random</b>          | 0.46                    | 0.44   | 0.66   | 0.5    | 1.95   | 2      |                                   |                                  |                      |                       |                        |

All copper films show tensile stress after one dielectric bake cycle

MicroFab SC Process B differentiated in terms of lower tensile stress and strong texture

MicroFab Process D differentiated by elongation after first bake cycle and lowest impurities

Random orientation values 16% and above mean that direction has more crystallites oriented in that direction. This would indicate that MICROFAB SC Process B is strongly <210> textured with the majority of the crystallites favoring that orientation, based on a Times random value of 5.72 (The Times random range is from 0 to 6). The other processes are mostly random. In addition, MICROFAB SC Process B is relatively stress neutral when compared against the other process which have become more tensile upon annealing. For the most part, the crystallite size is not affected much by the purity of the process. The tendency is toward formation of large grains post annealing.

# Summary III



- **The electrolyte must be carefully chosen to fulfill the requirements of many applications:**
  - Electrochemical data have shown its composition is important for controlling deposition rate, and macro-uniformity
- **For the accelerator, it is imperative to gauge its operating window so adequate polarization can be achieved and controlled.**
  - Its interaction especially with the leveler component is extremely critical
- **The suppressor component is most critical to establish proper nucleation necessary for determining bump shape:**
  - This nucleation might be important in providing relative adhesion
  - Further, a delicate balance must be established between leveler and suppressor
- **Leveler, the corner stone of any process:**
  - Its strength and type control parameters such as WID, WIF, gap fill capability, and the propensity for mitigating/controlling Kirkendall voids

# Desired Properties for WLP Copper Plating

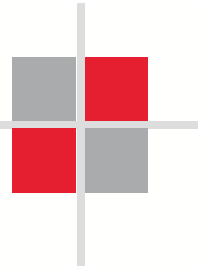


| Process           | [Cu] g/L | Accelerator | Suppressor  | Leveler     |
|-------------------|----------|-------------|-------------|-------------|
| <b>Megabumps</b>  | 50-90    | Strong      | Strong      | Strong      |
| <b>Pillars</b>    | 40-50    | Strong      | Weak-Strong | Strong      |
| <b>Microbumps</b> | 10-30    | Strong      | Strong      | Weak        |
| <b>RDL</b>        | 10-20    | Strong      | Strong      | Weak-Strong |
| <b>RDL + TSV</b>  | 40-50    | Weak        | Weak-Strong | Weak-Strong |



# Acknowledgements

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## R&D

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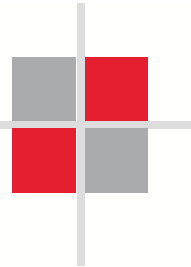
## Project Management

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## Outside Lab

X-ray Wizards

# WLP Product Summary



- Proliferation of WLP driven by specific cost, size and performance required by market
- Wafer Level Cu plating requirements continue to be pushed to limits

| Feature        | Critical Plating Attribute         | Diameter/ L/S   | Height    | Package Type | Cu pillar / RDL on | Application                   |
|----------------|------------------------------------|-----------------|-----------|--------------|--------------------|-------------------------------|
| Microbump      | Coplanarity , KV free              | <30um           | <20um     | 2.5D & 3D IC | Wafer              | HMC, FPGA                     |
| Cu pillar      | Coplanarity with higher throughput | 30-60um         | 30-50um   | FC & 2.5D    | Wafer              | CPU, APU, baseband, DDR4 DRAM |
| Cu pillar      | Coplanarity with higher throughput | 60-80um         | 50-70um   | FC & 2.5D    | Wafer              | Power Amplifier               |
| Large bump     | Higher Throughput                  | 90-110um        | 40-60um   | FC & 2.5D    | Wafer              | FPGA                          |
| High Cu Pillar | Coplanarity with higher throughput | 110-200um       | 130-180um | PoP          | Substrate          | Memory + AP / baseband        |
| Mega bump      | Higher throughput                  | 200um           | 200um     | 3D fan out   | Wafer              | Memory + AP / baseband        |
| RDL            | Coplanarity, Lines/Space control   | 1.5um/<br>1.5um | <2um      | Fan-Out      | Wafer              | Memory + AP / baseband        |
| 3 in 1         | All of the above                   | Broad range     | NA        | Several      | Wafer              | Mobile                        |

- Close collaboration between OEM, IDM, Foundry, OSAT, Chemistry supplier, Tool OEM required
- Mass Reflow vs. TCB driven by pitch/cost/performance trade-offs

